## **TFAWS Aerothermal Paper Session**





## A Plume Impingement Test for Code Validation

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Presented By

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Thermal & Fluids Analysis Workshop TFAWS 2012 August 13-17, 2012 Jet Propulsion Laboratory Pasadena, CA

#### **Outline**



- Overview of Plume Impingement Test Panel (PITP)
  - Risk Mitigation Task
  - Mechanical Design
  - Instrumentation
  - Fabrication
- PITP Installation and Test at Marshall Space Flight Center (MSFC) Solid Propulsion Test Area (SPTA)
- Solid Rocket Test Motor N2 (SRTMV-N2) PITP Test Data Assessment Status
  - Pressure Data
  - Thermal Data
  - TPS Recession
- SRTMV-N2 PITP Data Analysis, Documentation, and Computational Fluid Dynamics (CFD) Code Validation Plans



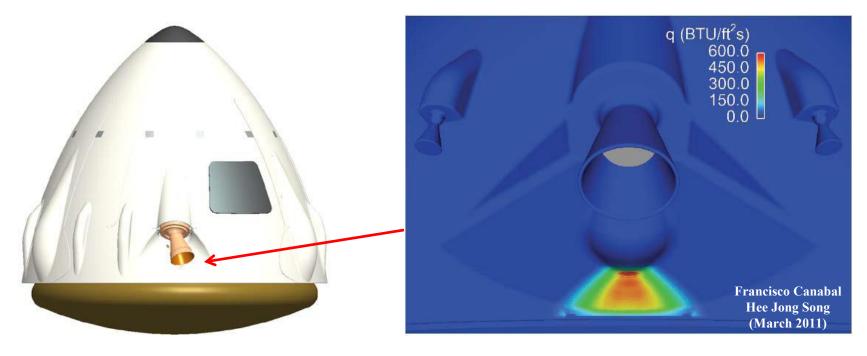


## Overview of PITP Risk Mitigation Task, Mechanical Design, Instrumentation, and Fabrication



## **Motivation for Risk Mitigation Proposal**





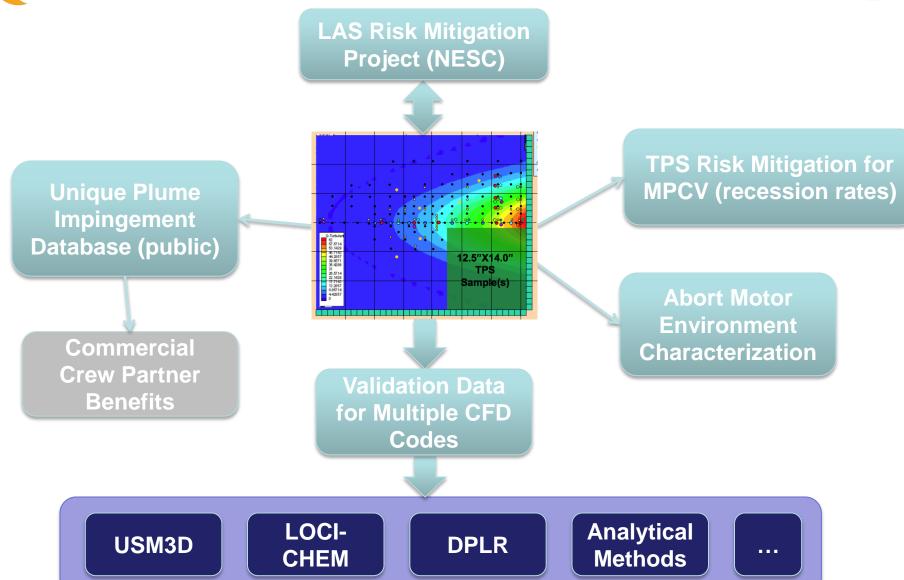
#### Risk Statements for Max Launch Abort System (MLAS) II (From 2/4/11):

- AERO-1: Given uncertainties associated with CFD modeling of hot plume exhaust products, there is a risk that the accuracy of the aerodynamics database could be reduced. (AERO)
- AERO-2: Given hot exhaust jet impingement from the AM exhaust...onto the surface of the fairing, there is a potential for hot plume impingement on the structure. (THERMAL)



#### **Impact of SRTMV-N2 Plume Impingement Panel Test**



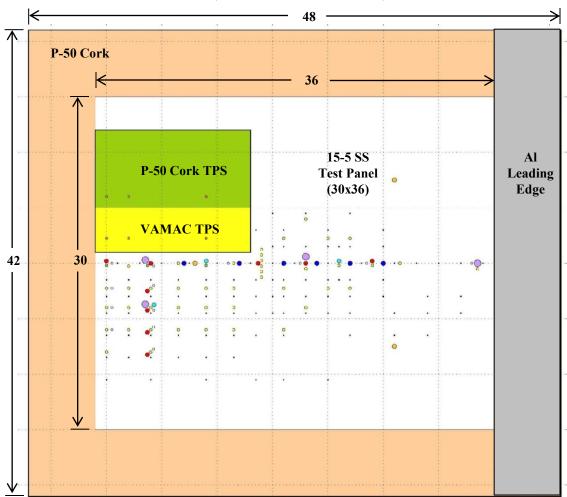


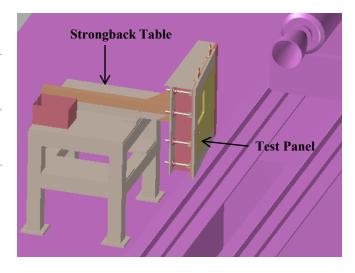


#### Design of the SRTMV-N2 Plume Impingement Test Panel









- Radiometer (4)
- Kulite (6)
- Accelerometer (3)
- Schmidt–Boelter Heat Flux (3)
- Gardon Heat Flux (9)
- Coaxial Tri–Thermocouple (3)
- Coaxial Thermocouple (43)
- Backside Thermocouple (13)
- · Static Pressure (96)
- TPS Type–K TC (12)



## **Instrument Naming Convention**



Naming Convention
iLLXX(p/n)YYdZ
i=Leading character ("i") to denote impingement plate instrument
LL=Abbreviation of Instrument type (see Below)
<b>XX</b> =Approximate X position in inches
(p/n)= Positive or negative associated with YY
YY=Approximate Y position in inches

**dZ**=Nondimensional depth, 0=surface, 5=backwall, if not specified use d0

Depth	
d0	Surface/Tri-Coax 1 (default)
d1	Tri-Coax 2
d2	Tri-Coax 3
d3	TPS 1
d4	TPS 2
d5	Backwall

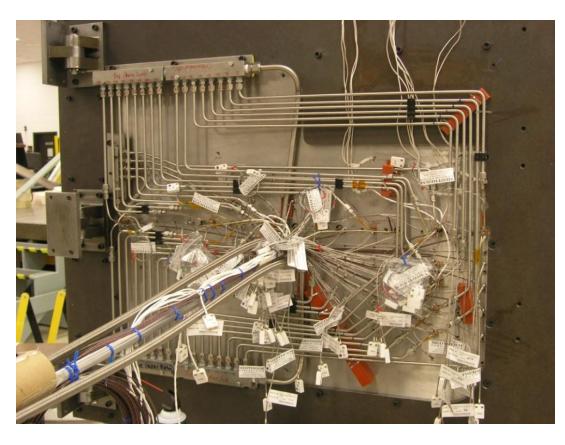
Abbre	Abbreviation				
SP	Static Pressure Tap				
UP	Kulite (Unsteady Pressure)				
CQ	Coaxial Thermocouple				
GQ	Gardon Heat Flux Gage				
RQ	Radiometer				
AN	Accelerometer (Normal)				
AT	Accelerometer (Tangential)				
CT	Coaxial Tri-Thermocouple				
SQ	Schmidt-Boelter Heat Flux				
ВТ	Backside Thermocouple				
TT	TPS Type K Thermocouple				

Tri-coaxial Thermocouple Naming Convention					
	(EXAMPLE: iCT35n00d2)				
i	Panel Test Instrument				
СТ	Tri-coaxial Thermocouple				
35	approximate downstream distance from the panel leading edge (inches)				
n	Below (not on) the centerline				
00	approximate spanwise distance from the panel centerline (0 - 0.5 inches)				
d2	0.060" below the surface				



## **PITP Instrumentation Photos**





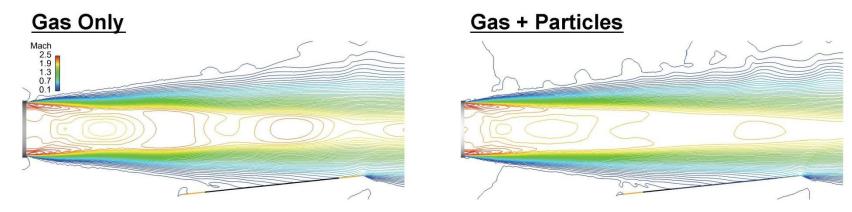




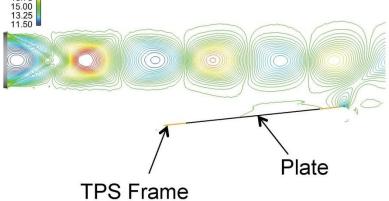
#### **Loci-CHEM Pre-Test Predictions**



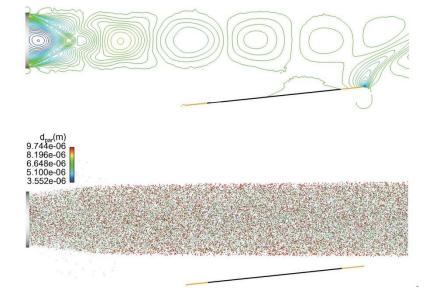
#### **Plume Distributions**



PITP Leading Edge at X=47.75", Y=16.8"; Angle=6°



CFD Analysis: Francisco Canabal – MSFC EV33





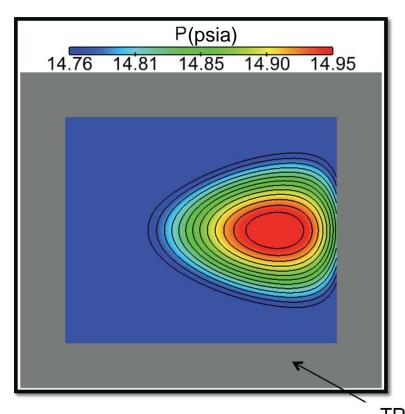
#### **Pre-Test Loci-CHEM Predictions**

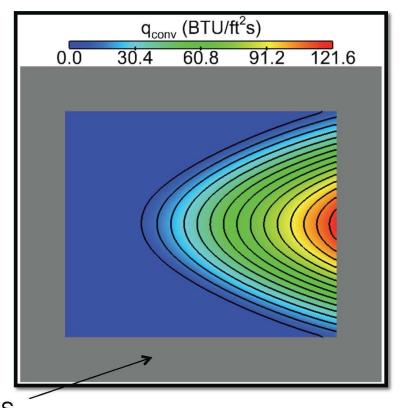


## Plate Surface Pressure and Convective Heat Flux Distributions

**Loci-CHEM (gas + particles)** 

Flow Direction





PITP Leading Edge at X=47.75", Y=16.8"Angle=6°



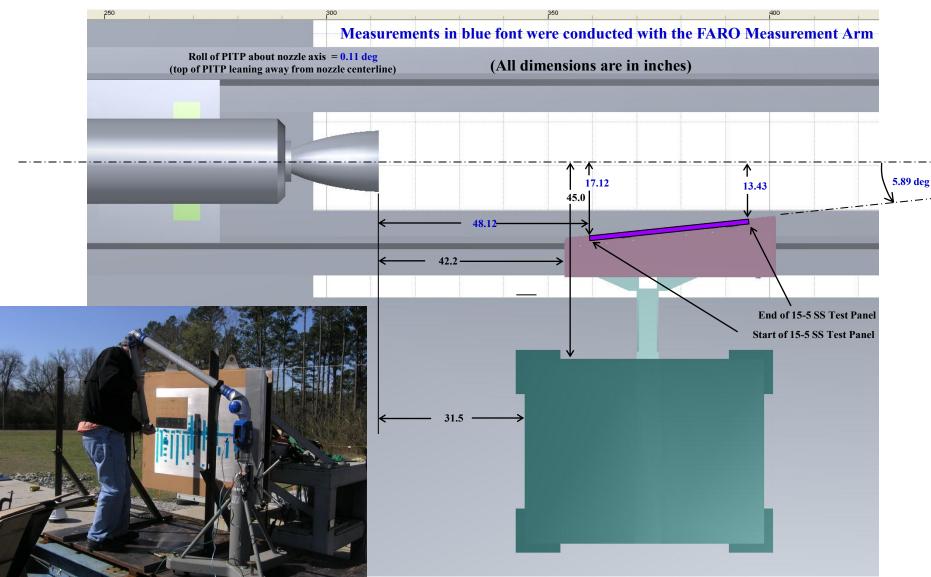


# PITP Installation and Test at MSFC SPTA



### **PITP Position (Planform View)**



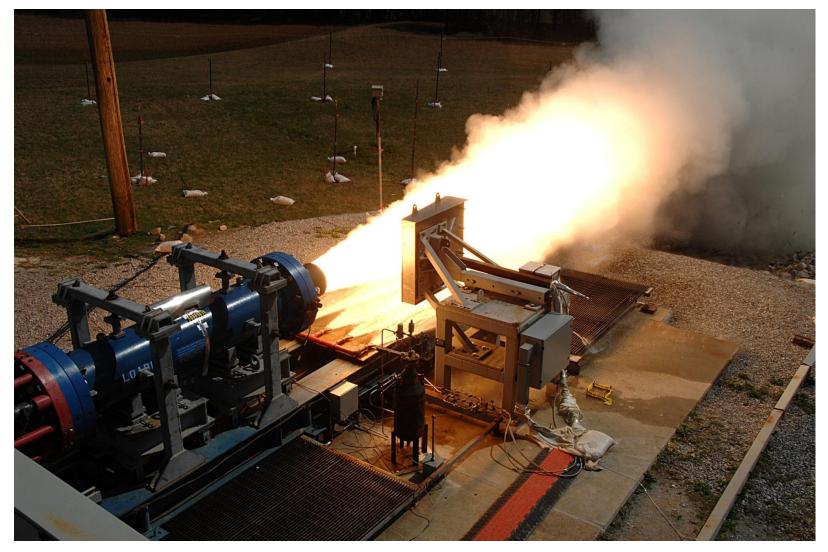




## **SRTMV-N2 PITP Test Video**



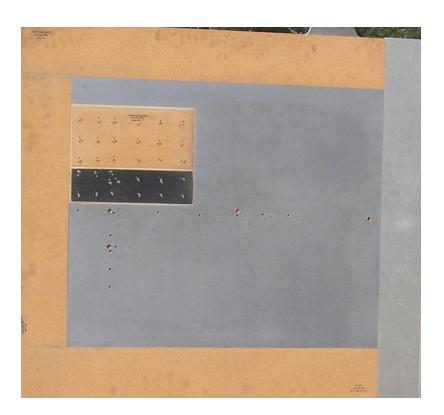
#### **CLICK PICTURE TO START VIDEO**

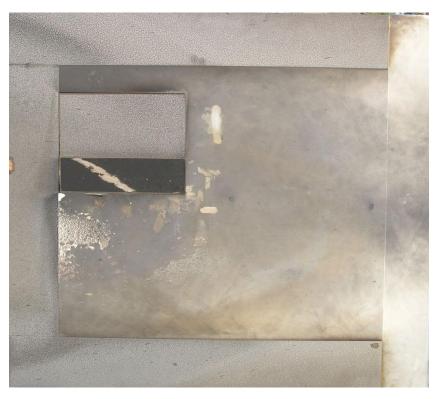




### **Test Panel – Before and After**







Post-test examination of the panel revealed significant recession of both the P-50 cork and VAMAC thermal protection materials. Aluminum deposition occurred below the plate centerline near the back end of the panel.





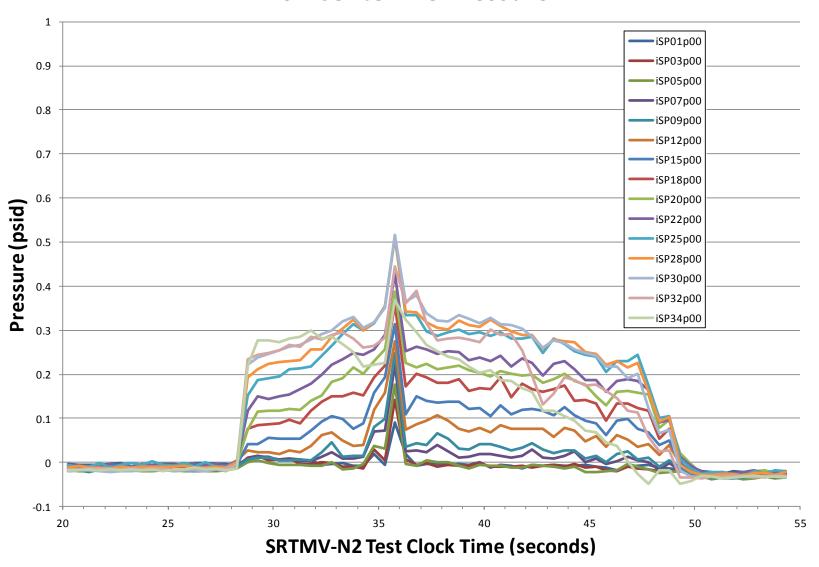
# SRTMV-N2 PITP Test Preliminary Pressure Data Assessment



### **Centerline Pressure Data**



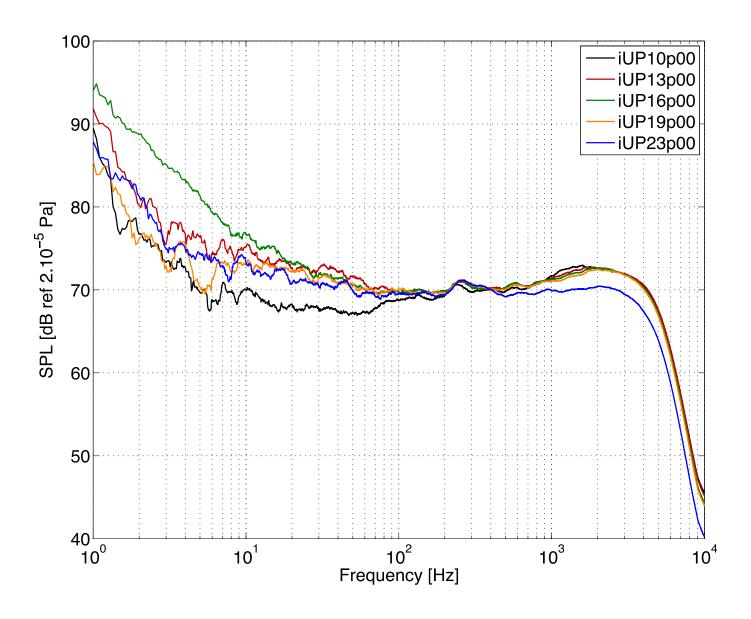
#### **iSP Centerline Pressure**





## **SRTMV-N2 PITP Unsteady Pressure**









# SRTMV-N2 PITP Test Preliminary Thermal Data Assessment



## **Thermal Analysis Overview**



#### Gardon & **Back wall Radiometers** Coaxial Tri-Coaxial Schmidtthermocouples **Thermocouples Thermocouples Boelter Heat** Analytical Methods Heat Flux **Heat Flux Temperature Temperature** boundary SINDA boundary boundary boundary condition condition condition condition **Temperature Temperature** Cook's Boundary Boundary Method condition condition Heat **Temperature** Conduction gradient **Equation**



**Semi-Infinite** 

**Wall Solution** 

Lump

Capacitance

Model

Initial and final

temperature

conditions

indicates that the measurement is not required as part of the analytical solution, but can be compared to the analytical result

Initial and final

temperature

conditions

Heat Flux

boundary

condition

Heat Flux

boundary

condition

Initial and final

temperature

conditions



#### **Types of Heat Flux Measurements**



#### Direct Measurements

- Gardon Gages (9 instruments)
- Schmidt-Boelter Gages (3 instruments)
- Radiometers (4 instruments)

#### Indirect Measurement

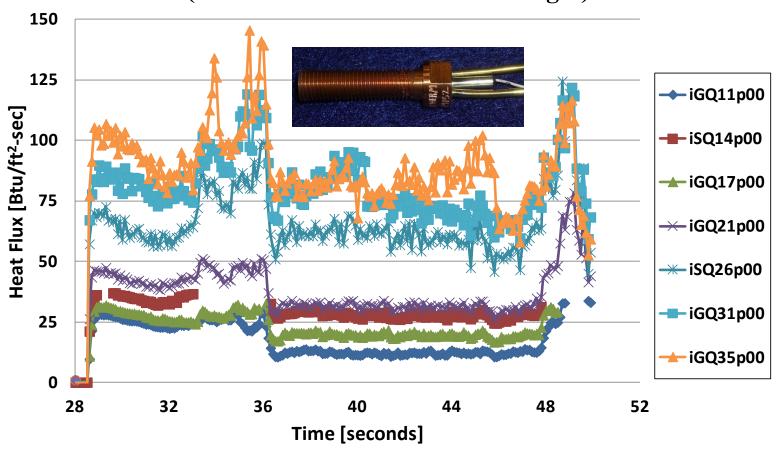
- Heat Conduction via tri-coaxial thermocouple probe (3 instruments)
- Analytical method using surface coaxial thermocouple measurements (43 instruments)



#### **Centerline Heat Flux**



#### (Gardon & Schmidt-Boelter Gages)



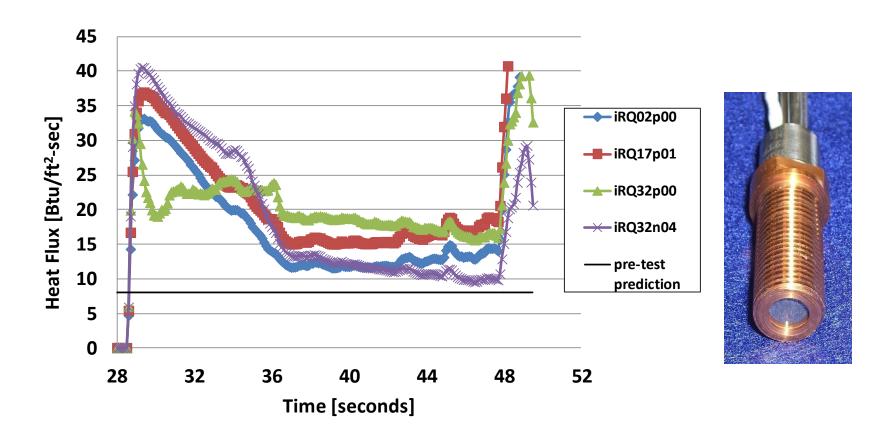
Due to the position of the plate, higher heat fluxes were predicted for the rear portion of the plate. Measurements agreed with predictions.

(Schmidt-Boelter gage (Station 14) provided an unexpected elevated reading)



#### **Radiometers**



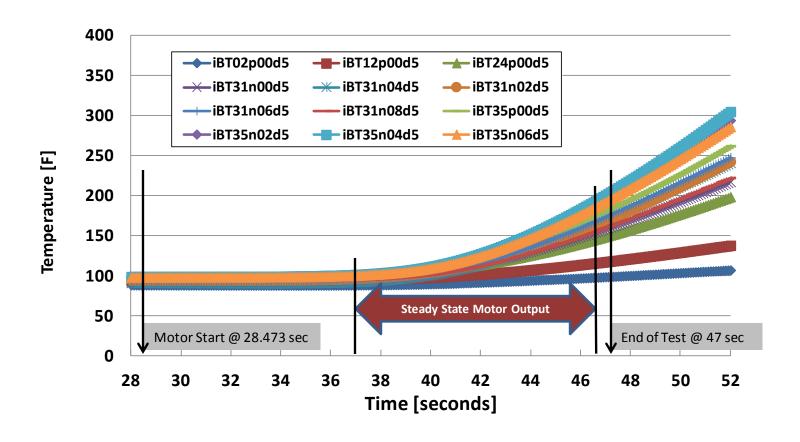


Radiometers over-ranged at both the start and the end of the test (design limit set to 30 Btu/ft<sup>2</sup>-sec).



## **Panel Back Wall Temperatures**





Back wall temperatures measurements do not respond appreciably until near the end of the motor burn.



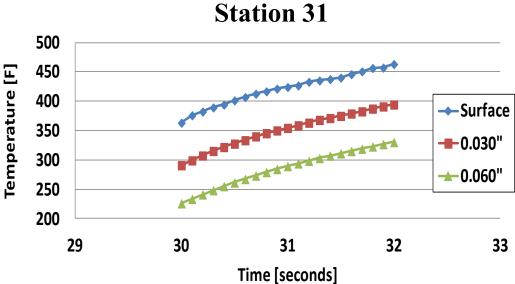
## **Tri-coaxial Thermocouples**



Tri-coaxial thermocouples measured material temperature at three different depths (0, 30, & 60 mils) and indicated that a well behaved thermal gradient was established through the material.

Heat conduction estimates for the tri-coaxial thermocouples matched heat flux gage measurements.

Time	Surface	30_mils	60_mils		Delta1	Delta2	DeltaT
30.0	362.8	290.4	225.3		72.4	65.1	137.5
30.2	382.0	306.9	240.6		75.1	66.3	141.4
30.4	392.9	321.6	254.7		71.3	66.9	138.2
30.6	406.5	333.1	267.2		73.4	65.9	139.3
30.8	417.1	345.4	278.8		71.7	66.6	138.3
31.0	422.9	354.4	289.0		68.5	65.4	133.9
31.2	435.7	363.0	298.3		72.7	64.7	137.4
31.4	438.7	371.5	307.1		67.2	64.4	131.6
31.6	446.9	379.1	315.1		67.8	64.0	131.8
31.8	455.0	387.2	322.5		67.8	64.7	132.5
			DT	R	70.8	65.4	136.2
			Dx	ft	0.0025	0.0025	0.005
			k	Btu/sec-ft-R	0.002873	0.002873	0.002873
			q	BTU/ft²-sec	81.35	75.16	78.25



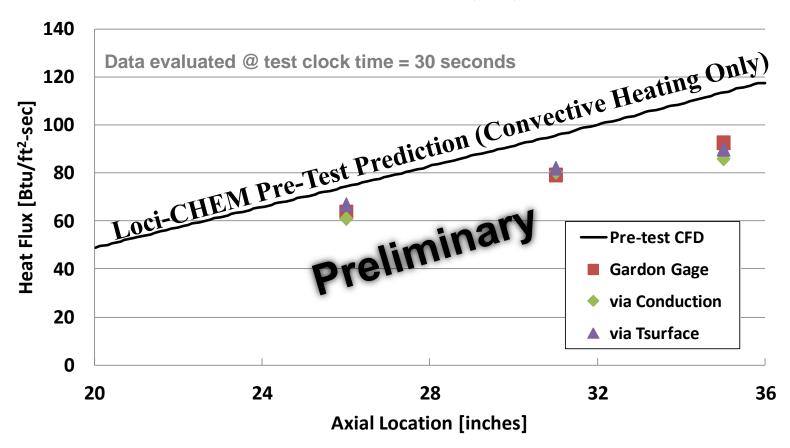




### Centerline Heat Flux Comparisons (all methods)



#### **Stations 26, 31, 35**

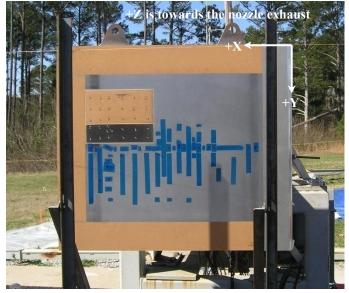


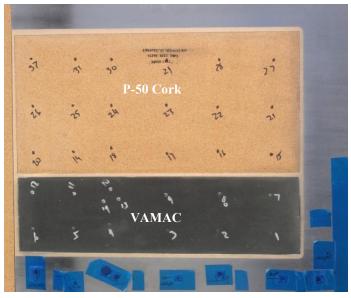
Good agreement was achieved among analytical methods.



## **TPS Surface Point Measurements (Pre Test)**







VAMAC Surface Survey Points					
Pretest					
Point ID#	Х	Υ	Z		
1	29.559	18.836	-0.053		
2	32.071	18.754	-0.054		
3	34.493	18.769	-0.053		
4	37.292	18.470	-0.053		
5	39.088	18.655	-0.065		
6	41.074	18.717	-0.071		
7	29.577	17.003	-0.039		
8	31.952	16.931	-0.035		
9	34.548	16.972	-0.026		
10	37.248	16.712	-0.031		
11	39.008	16.944	-0.048		
12	41.091	16.912	-0.065		
13	36.812	17.179	-0.031		
14	37.578	17.303	-0.035		

P-50 Cork Surface Survey Points					
Pretest					
Point ID#	X	Υ	Z		
15	29.486	15.041	-0.020		
16	32.038	14.877	-0.009		
17	34.469	14.952	-0.002		
18	37.187	14.716	-0.005		
19	39.017	14.917	-0.023		
20	40.990	14.937	-0.046		
21	29.474	12.770	-0.018		
22	32.049	12.726	-0.008		
23	34.516	12.674	-0.004		
24	37.146	12.681	-0.005		
25	39.024	12.689	-0.019		
26	40.999	12.738	-0.044		
27	29.392	10.537	-0.019		
28	31.983	10.529	-0.017		
29	34.489	10.498	-0.017		
30	37.152	10.483	-0.022		
31	38.902	10.446	-0.035		
32	41.085	10.422	-0.050		



## **TPS Surface Point Measurements (Post Test)**





#### **Post Scrape - Char Layer Removed**

VAMAC Surface Survey Points					
Post-Test with Char Removed					
Point ID#	Х	Υ	Z		
1	29.559	18.836	-0.227		
2	32.071	18.754	-0.246		
3	34.493	18.769	-0.270		
4	37.292	18.470	-0.304		
5	39.088	18.655	-0.334		
6	41.074	18.717	-0.362		
7	29.577	17.003	-0.181		
8	31.952	16.931	-0.191		
9	34.548	16.972	-0.216		
10	37.248	16.712	-0.245		
11	39.008	16.944	-0.293		
12	41.091	16.912	-0.335		
13	36.812	17.179	-0.249		
14	37.578	17.303	-0.275		

P-50 Cork Surface Survey Points					
Post-Test with Char Removed					
Point ID#	Х	Υ	Z		
15	29.486	15.041	-0.236		
16	32.038	14.876	-0.261		
17	34.469	14.952	-0.301		
18	37.187	14.716	-0.332		
19	39.017	14.917	-0.390		
20	40.990	14.937	-0.448		
21	29.474	12.770	-0.172		
22	32.049	12.726	-0.185		
23	34.516	12.674	-0.209		
24	37.145	12.680	-0.255		
25	39.024	12.689	-0.304		
26	40.998	12.738	-0.348		
27	29.392	10.537	-0.141		
28	31.983	10.529	-0.153		
29	34.489	10.498	-0.172		
30	37.152	10.483	-0.206		
31	38.902	10.445	-0.226		
32	41.085	10.422	-0.268		



## **Key Data Observations**



- Instrument readings and video suggest that significant variations in both plume shape and motor thermal output occurred after T+3 seconds into the test. This event is still unexplained but good data exists prior to 3 seconds.
- Particle plume impingement was not expected to occur on the test article
  - Heat flux measurements were inline with pre-test CFD heating
  - Significant Aluminum deposition was observed between Stations 30 to 36
- The thermocouple array at Station 21 and post-test inspection of the panel (aluminum deposition and burn patterns) indicated that the plume centerline was an inch or more below the panel centerline, likely after T=3 seconds
- Initial data inspection appears to indicate that the best data for CFD comparison is prior to the peak transient event (T=1-3 seconds)
- The measured radiative heating was higher than expected and is being investigated
- Nearly all instrumentation survived the test, performed as expected and are reusable with standard refurbishment
- TPS sample recession was measurable and significant but less than predicted
  - Using Shuttle Heritage TPS Recession Rates





# SRTMV-N2 PITP Data Analysis, Documentation, and CFD Code Validation Plans



## **PITP Data Analysis Plans**



- Full spatial inspection and analysis of all streamwise and spanwise pressure and thermal test data from the PITP
  - Nearly Complete
- Analysis of all test data before and after the transient peak event for potential CFD comparison
  - Nearly Complete
- Examination of radiometer over-ranged data
  - Post-test calibration of radiometers is in progress and will be completed very soon
- Analysis of IR camera video data
- Analysis of temperature and erosion data from the VAMAC and P50 Cork TPS coupons (MPCV effort)



## **CFD Analysis Plans**



#### Post-Test SRTMV-N2 Nozzle Test Conditions (SRTMV-N2 Funded):

- Post-Test Nozzle QA : COMPLETE
- ◆ Computation of Nozzle Geometry vs Test Time : COMPLETE
- Computation of Nozzle Test Conditions vs Time : COMPLETE

#### Post-Test CFD (MLAS Funded):

- ◆ Engineering Code Analysis of SRTMV-N2 Nozzle : COMPLETE
  - Nozzle exit conditions for CFD : COMPLETE
  - **♦** Loci-CHEM CFD (Francisco Canabal, MSFC) : IN PROGRESS
    - USM3D (Erik Tyler, LaRC): IN PROGRESS

#### Post-Test CFD (MPCV Aerosciences Funded, Rick Thompson):

- VULCAN (Tom Jentink, LaRC)
- FUN3D (Victor Lessard, LaRC)
- Loci-CHEM (Alireza Mazaheri, LaRC)



### **SRTMV-N2 PITP Documentation Plans**



#### SRTMV-N2 PITP Test Report

- PITP hardware, instrumentation, test conduct, and test data
- A NASA/NESC archival document

#### CFD Assessment for SRTMV-N2 PITP Test Data

- An assessment of the multiple CFD codes and their results compared to the test data
- A NASA/NESC archival document



### **Team Membership for PITP Risk Mitigation Task**



Research Team Members

David Witte (LaRC)

Jeremy Pinier (LaRC)

Jason Mishtawy (MSFC)

Bud Smith (MSFC)

Vince Cuda (LaRC)

Francisco Canabal (MSFC)

Erik Tyler (LaRC)

Tom Jentink (LaRC)

Darrel Davis (MSFC)

Stan Bouslog (JSC)

Scott Coughlin (JSC)

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Jeremy Kenny (MSFC)

Sam Yunis(LaRC)

Sandy Webb (LaRC)

Dave Castle (LaRC)

Tom Hall (LaRC)

Wayne Geouge (LaRC)

Rick Irby (LaRC)

Jeff Petty (LaRC)

Dennis Strickland (MSFC)

Jason Elmore (MSFC)

Ernie Wooten (MSFC)

Scott Ringel (MSFC)

Darrell Gaddy (MSFC)

Responsibility

FTV-2 Aero Lead / PITP PM

FTV-2 Deputy Aero Lead

Research Lead

Aerothermal Loads

Thermal Analysis / Instrumentation

CFD (Loci CHEM)

CFD (USM3D)

CFD (VULCAN)

**TPS Research** 

**TPS Research** 

**TPS** Research

Role

Guidance/Test Expertise

Structural Dynamics Support

Mechanical Design

Mechanical Stress Analysis

Instrumentation Installation Lead

Instrumentation Installation

Instrumentation Support Systems

Pressure Scanner DAS

SPTA Facility Manager

SPTA Data Acquistion

SPTA Instrumentation

SRTMV-N2 Design Lead

IR Cameras



## **Questions?**



